

INFLUENCE OF REACTIVE AND MAXIMUM STRENGTH INDICATORS ON SPRINT  
PERFORMANCE

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Healy, R., Smyth, C., Kenny, I.C., and Harrison, A.J. (2018) 'Influence of reactive and maximum strength performance indicators on sprint performance. *Journal of Strength and Conditioning Research*. [Epub ahead of print] (DOI: 10.1519/JSC.0000000000002635).

## **ABSTRACT**

The primary aim of this study was to assess the relationship between reactive and maximal strength measures with 40 m sprint performance and mechanical properties. Fourteen male and fourteen female sprinters participated in this study. On the first day subjects performed 40 m sprints with 10 m split times recorded in addition to maximal theoretical velocity, maximal theoretical force and peak horizontal power which were calculated from force-velocity relationships. On the second day subjects performed isometric mid-thigh pulls (IMTP) with peak force and relative peak force calculated, drop jumps and vertical hopping where the reactive strength index (RSI) was calculated as jump height (JH) divided by contact time (CT). Pearson correlations were used to assess the relationships between measures and independent samples t-tests were used to assess the differences between men and women. No significant correlations were found between drop jump and hopping RSI and sprint measures. A significant strong positive correlation was found between IMTP peak force and peak horizontal power in men only ( $r = 0.61$ ). The male sprinters performed significantly better in all recorded measures apart from hopping (CT, JH and RSI) and drop jump CT where no significant differences were found. The lack of association between reactive and maximal strength measures with sprint performance are potentially due to the test's prolonged CTs relative to sprinting and the inability to assess the technical application of force. Several methods of assessing reactive strength are needed that can better represent the demands of the distinct phases of sprinting e.g. acceleration, maximum velocity.

**KEY WORDS:** drop jump, hopping, isometric mid-thigh pull, stretch shortening cycle, contact time, force-velocity profiling.

## INTRODUCTION

Sprint performance is critical to success in various team and individual sports. In track events, rapid acceleration and high maximum velocity are crucial to race performance (20, 35). The 100 m sprint can be broken down simply, into three main phases: the acceleration phase, the maximum velocity phase and the deceleration phase (9). Furthermore, each phase can be sub-divided in various ways e.g. the initial acceleration phase (0-12 m) and the main acceleration phase (12-35 m) (21). Consequently, sprinting can be considered a multidimensional skill with different kinematic and kinetic requirements during the distinct phases (9). Accordingly, different strength capabilities play relatively larger roles throughout the performance of a sprint (26).

A novel field method of profiling athletes' horizontal force-velocity relationship over 40 m has recently been developed (32). Mechanical variables such as the theoretical maximum horizontal component of ground reaction force ( $F_0$ ), theoretical maximum horizontal velocity ( $v_0$ ) and the maximum horizontal mechanical power ( $P_{max}$ ) produced can all be measured during accelerative performance (32). Research on sprint athletes has found that maximum velocity and mean 100 m velocity were both very strongly correlated with  $P_{max}$  (23). In contrast, Slawinski et al. (35) found no correlation between  $P_{max}$  and 100 m time, whereas  $v_0$  had a very large negative correlation with  $P_{max}$  in world class athletes. It is suggested that  $P_{max}$  may be more likely related to performance over shorter distances i.e. 40 or 60 m where fatigue is limited (35). This is supported by Rabita et al. (28) who found that maximal velocity achieved over 40 m and 40 m performance in elite and sub elite sprinters had an almost perfect positive and very large positive correlation with  $P_{max}$  and  $v_0$  respectively.

The ground contact phase of sprinting involves the coupling of an eccentric contraction with a concentric contraction. This is termed the stretch shortening cycle (SSC) and it is frequently used in many additional sports movements; e.g. in the leg extensor muscles during jumping and hopping (27). The SSC has been classified as either fast, where contact times (CTs) < 0.250 s, or slow, where CTs > 0.250 s (34). Therefore, sprinting is considered a fast SSC activity as a sprinter's CT after the initial block push off, is below 0.250 s for each step with CTs progressively decreasing throughout the acceleration phase with values as low as ~0.090-0.120 s reported at maximum velocity (8, 19). Traditionally, fast SSC performance has been assessed through the measurement of the reactive strength index (RSI) which is

usually calculated by dividing the jump height by the contact time in a specific jump (45). The RSI has been assessed during drop jumps, rebound jumps and ankle jumps (hopping) (13, 26, 46).

The association between RSI and sprint performance in sprint athletes has been previously studied with contrasting results. Young et al. (46) found no relationship between 2.5 m and 50 m sprint times and drop jump RSI in male and female sprinters. In contrast, Hennessy and Kilty (15) found very large negative correlations between sprint times over 30 m and 100 m and RSI in female sprinters. Furthermore, Smirniotou et al. (36) found moderate to large negative correlations between sprint performances over 10, 30, 60 and 100 m and drop jump RSI in male sprinters. Nagahara et al. (26) assessed RSI during rebound jumps (termed the “rebound jump index”) and bilateral vertical hops (termed the “ankle jump index”) along with sprint time and individual step acceleration over 60 m. Although rebound jump RSI was not related to any of the sprint measures, hop RSI had a moderate negative relationship with 60 m time and a moderate to large positive relationship with step acceleration over the 23 – 34 m interval. Additionally, Nagahara et al. (26) found no relationship between rebound jump RSI and hop RSI. The relationship between hop RSI and drop jump RSI has yet to be assessed. This warrants investigation as Hop RSI may provide coaches with an additional insight into the reactive strength capabilities of their athletes.

Sprinting requires the production of very large forces over very short time periods. Consequently, sprint coaches utilize a variety of training modalities to develop different strength qualities; these may include reactive strength and maximum strength training performed throughout the training cycle (5). Maximum strength has been defined as the ability to voluntarily generate maximal force under specified conditions (29). Strength tests such as the back squat and isometric squat have previously been used with sprint athletes with very strong negative correlations found between relative 1RM and 100 m time (22) and between peak force (PF) and maximum velocity (46). The isometric mid-thigh pull (IMTP) has become a popular method of assessing maximum strength as the peak force applied during the pull can be measured directly from a force platform. Several authors have assessed peak force and relative peak force measured in an IMTP with sprint performance in team sport athletes with contrasting results. Significant relationships have been found between PF and 5 and 20 m times (39) and between relative PF and 10 m time (41, 42). Wang et al. (41) however, found no relationship was found between PF and short sprint performance (5 m and

10 m). It is not currently known whether stronger sprint athletes, as measured by the IMTP, produce higher levels of maximal mechanical power or apply greater maximal theoretical horizontal forces during a sprint.

The primary aim of the current study was to assess the relationship between maximal strength, reactive strength, as measured in vertical hopping and drop jumping, and sprint performance. A secondary aim was to evaluate the differences between male and female sprinters' maximal strength, reactive strength and sprint performance.

## **METHODS**

### **Experimental Approach to the Problem**

A cross sectional research design was undertaken over two days of testing. On day one subjects performed 40 m sprints on an indoor athletic track. Sprint mechanical properties  $F_0$ ,  $v_0$ ,  $P_{\max}$  and max velocity were calculated in addition to split times from 0-10 m, 10-20 m, 20-30 m and 30-40 m and 40 m sprint time. On the second day of testing peak force and relative peak force values were measured during isometric mid-thigh pulls and CT, JH and RSI measures were calculated during drop jumps and vertical hopping tests. All testing on day two was performed in a biomechanical laboratory. Test days were separated by no longer than seven days.

### **Subjects**

Twenty eight sprinters consisting of fourteen men (mean  $\pm$  SD, age:  $22 \pm 2$  years; body height:  $1.82 \pm 0.07$  m; body mass:  $73.1 \pm 6.8$  kg) and fourteen women (mean  $\pm$  SD, age:  $22 \pm 4$  years; body height:  $1.72 \pm 0.07$  m; body mass:  $64.4 \pm 4.6$  kg) agreed to participate in this investigation. Fifteen of the athletes competed regularly at an international level (seven men and eight women) while the remaining thirteen athletes competed regularly at a national level (seven men and six women). All athletes had at least two years of sprint and plyometric training experience. The athletes' regular weekly conditioning programme consisted of 3 – 4 sprint training sessions which included a mixture of technical, acceleration, maximum speed and speed endurance sessions. Athletes typically performed two conditioning sessions a week distinct from sprinting sessions which included a mixture of hurdle jump, medicine ball, bounding and hopping exercises in addition to conventional strength training exercises and

variations e.g. Romanian deadlifts. Ethical approval was provided by the Institution's Research Ethics Committee. Additionally, athletes were informed of the benefits and risks of the investigation and written consent forms were completed prior to testing in compliance with the Declaration of Helsinki.

## 40 m Sprint Testing

Following an individualized, race specific warm up, lasting ~30 minutes, athletes completed three maximal effort 40 m sprints from a block start with the first trial acting as a familiarization trial. Six minutes of recovery time were provided with additional time granted if requested. To ensure athletes continued sprinting at maximal effort for the entire 40 m, coloured cones were placed at 45 m and athletes were instructed not to begin their deceleration until they had passed the cones. Racetime 2, dual-beam timing gates (Microgate, Bolzano, Italy) were positioned at 10 m, 15 m, 20 m, 30 m and 40 m. Split times from 0-10 m, 10-20 m, 30-40 m, and overall 40 m were recorded in addition to maximal velocity which was calculated as the fastest 10 m split time divided by 10. Timing was initiated at the instant the athlete's hand left the track surface using a previously validated protocol which synchronised timing gates to the Optojump™ system which is an optical measuring unit (14). This protocol enabled the measurement of the true 10 m movement time.

In addition to sprint performance measures, sprint mechanical properties were calculated based on the five timing gate split times using the methods of Samozino et al. (32). The horizontal velocity of the center of mass ( $v_h$ ) versus time (t) curve was modelled using a mono-exponential function (32):

$$v_h(t) = v_{hmax} \cdot (1 - e^{-t/\tau}) \quad \text{Eq. 1.}$$

where,  $v_{hmax}$  is the maximal velocity, t is the time and  $\tau$  is the acceleration time constant which represents the ratio of maximal velocity to maximal acceleration. By integrating equation 1, an equation for the horizontal position of the center of mass can be derived:

$$x_h(t) = v_{hmax} \cdot \left( t + \tau \cdot e^{-\frac{t}{\tau}} \right) - v_{hmax} \cdot \tau \quad \text{Eq. 2.}$$

Using equation 2 and the Microsoft Excel Solver function, the best approximations of  $v_{hmax}$  and  $\tau$  were calculated using a least squares approach between the raw position time data, collected from the timing gates, and the modelled position time data. The approximated  $v_{hmax}$  had a near perfect correlation with the maximum velocity recorded during the sprints ( $r = 0.992$ ,  $ICC = 0.99$ ). Once  $v_{hmax}$  and  $\tau$  values were approximated, horizontal velocity time curves could be derived using equation 1. Velocity time curves were subsequently differentiated once with respect to time to give acceleration time curves  $a_h(t)$ .

$$a_h(t) = \left(\frac{v_{hmax}}{\tau}\right) \cdot e^{-\frac{t}{\tau}} \quad \text{Eq. 3.}$$

The net horizontal component of ground reaction force (GRF) applied to the center of mass was modelled over time as follows:

$$F_h(t) = m \cdot a_h(t) + F_{aero}(t) \quad \text{Eq. 4.}$$

Where  $m$  is the body mass of the sprinter and  $F_{aero}(t)$  is the estimated aerodynamic drag force the sprinter experienced throughout the sprint (2, 32, 40). The maximal theoretical horizontal velocity ( $v_0$ ) and maximal theoretical horizontal force ( $F_0$ ) were calculated as the x and y intercept of the individual force-velocity relationships, determined via least squares regression, respectively (24, 32). The  $F_0$  represents the maximal theoretical horizontal force applied by the athlete at the initial push i.e. when velocity is zero. The  $v_0$  represents the maximal theoretical horizontal velocity of the athlete if net internal and external mechanical resistances, such as drag, were null (24, 32). The maximum mechanical power developed in the horizontal direction ( $P_{max}$ ) was calculated using the following equation validated by previous work (31, 33):

$$P_{max} = \frac{F_0 \cdot v_0}{4} \quad \text{Eq. 5.}$$

Both  $F_0$  and  $P_{max}$  were expressed relative to body mass.

### **Isometric Mid-Thigh Pull**

A specific IMTP warm up, consisting of pulling the IMTP bar at an intensity of 50%, 70% and 90% for a period of five seconds, was performed by each athlete (4). The height of the

IMTP bar was set individually so that each athlete could adopt the second pull position of the clean with an upright trunk and knee angle  $\sim 130\text{-}140^\circ$  (12, 38). Following the warm up, athletes performed two maximal effort pulls separated by 3 minutes of rest. Athletes were instructed to adopt the second pull position and on the experimenter's verbal command of "GO!", to pull as hard and as fast as possible for the full five seconds (12). IMTP testing was conducted with a custom-made isometric rack (Odin, Ireland) that enabled the placement of a steel bar at intervals of 50 mm. The rack was anchored to the laboratory floor and placed over two AMTI force platforms (Advanced Mechanical Technologies, MA, USA) operating at 1,000 Hz. PF was calculated directly from the force-time curve as the maximum force produced during each five second trial. Relative PF was also calculated by dividing PF by the athlete's mass.

### **Drop Jumps**

Following a standardised dynamic warm up, athletes performed three maximal effort drop jumps with the first jump serving as a practice trial and the two subsequent jumps retained for analysis. Athletes were instructed to keep their hands on their hips throughout the entire movement, to step directly off of the box i.e. avoid stepping down from the box or jumping off of the box, avoid any tucking motion in the air and to attempt to land in the same position as take-off. Additionally, athletes were instructed to aim to minimise CT while also trying to maximise JH during each jump (45). All drop jumps were visually assessed by the experimenter and trials were repeated if any of the instructions were not correctly followed or if  $CT > 0.250$  s. Thirty seconds of rest were provided between trials to avoid any deleterious effects of fatigue on performance. Drop jumps were performed from a box height of 0.3 m with athletes landing on a force platform operating at 1,000 Hz.

The dependent variables calculated were: CT, JH and RSI. CTs were obtained directly from the force-time trace using a threshold of  $>10$  N to determine contact and  $<10$  N to determine flight. Flight time i.e. the time elapsed between the initiation of the flight phase and the subsequent contact phase was used to estimate JH using an adapted version of the second mathematical equation of linear motion i.e.  $JH = FT^2 \times 1.22625$ . RSI was calculated as JH divided by CT (45). The trial with the highest RSI was considered the best trial and was used for the final analysis.



## **Hopping Test**

For the hopping test, participants performed two trials of a 10 s hopping test at a frequency of 2.2 Hz. A 2.2 Hz hopping frequency was chosen as this frequency elicits shorter CTs and greater ankle stiffness compared to unconstrained hopping and hopping at lower frequencies e.g. 1.5 Hz (10, 16, 25). The hopping frequency was imposed via a metronome operating at 132 beats per minute. Participants were instructed: to land on the audible tone of the metronome, in the same position as take-off, to keep their hands on their hips throughout and to keep their legs as straight as possible by trying to avoid knee and hip flexion as much as possible (26). All trials were visually assessed by the same investigator to ensure consistent technique and remove invalid trials (i.e. where participants did not land on the force platform or took their hands off their hips). Similar to previous investigations, only hops that were performed within 2% (2.16 – 2.24 Hz) of the desired hopping frequency were included in the analysis (11). Similar to the ten to five repeated jump test, the five best hops, as determined by the highest RSIs, in each trial were used to calculate average values for CT, JH and RSI (13). Dependent variables were calculated using the same methods described for the drop jumps.

## **Statistical Analyses**

All variables were found to be normally distributed as the Shapiro-Wilk's test had an alpha level  $> 0.05$ . Descriptive statistics for all variables were presented as mean  $\pm$  SD. The test-retest reliability of each variable was assessed by calculating the single measure intraclass correlation coefficient (ICC) with 95% CI and the typical error, expressed as a coefficient of variation (CV%) (18).

Differences between men and women were assessed using independent samples t-tests and Cohen's d effect size (ES) was used to assess the magnitude of differences between groups. The absolute value of the effect sizes were interpreted as trivial ( $ES < 0.2$ ), small ( $0.2 \leq ES < 0.6$ ), moderate ( $0.6 \leq ES < 1.2$ ), large ( $1.2 \leq ES < 2$ ) very large ( $2 \leq ES < 4$ ) and extremely large ( $> 4$ ) according to the scale proposed by Hopkins et al. (17).

Relationships between sprint, reactive strength and maximal strength measures were determined using Pearson's product moment correlation with the alpha level set at 0.05. The strength of the correlations was evaluated as: trivial (0 – 0.09), small (0.1 – 0.29), moderate (0.3 – 0.49), large (0.5 – 0.69), very large (0.7 – 0.89), near perfect (0.9 – 0.99) and perfect

(1) (17). Non-significant correlations were not interpreted. All statistical analyses apart from the CV% were performed using SPSS software (version 21.0, SPSS, Inc., IL, USA).

## **RESULTS**

The results of the reliability analysis for sprint, IMTP, DJ and Hop measures are presented in Table 1. All measures displayed excellent reliability with ICCs above 0.90 (Range: 0.93 – 0.99) and CV% below <5% (Range: 0.3 – 4.9%). Descriptive statistics (mean  $\pm$  SD) for all variables in addition to mean differences between men and women and effect sizes are provided in Table 2. The men achieved significantly shorter sprint times, a greater maximum velocity and greater sprint mechanical properties with all effects being very large. No significant differences were found for any of the hop variables between men and women with effects considered trivial. Drop jump RSI and JH were significantly greater in men with moderate effect sizes. A small but non-significant effect was found in drop jump CT. Significantly greater IMTP PF and relative PF were found in men compared with women with effects considered large and moderate respectively.

Table 1: Test-retest single measure intraclass correlation coefficient with 95% CI and CV% for sprint, hop, drop jump and isometric mid-thigh pull for men and women.

		Men		Women	
		ICC	CV%	ICC	CV%
Sprint Performance	0-10 m (s)	0.93 (0.78 to 0.98)	0.7	0.99 (0.96 to 0.99)	0.6
	10-20 m (s)	0.93 (0.81 to 0.98)	0.8	0.98 (0.94 to 0.99)	0.6
	20-30 m (s)	0.96 (0.87 to 0.99)	0.6	0.99 (0.97 to 0.99)	0.5
	30-40 m (s)	0.98 (0.94 to 0.99)	0.6	0.99 (0.99 to 0.99)	0.4
	40 m (s)	0.98 (0.95 to 0.99)	0.4	0.99 (0.99 to 0.99)	0.3
	Max Velocity ( $\text{m}\cdot\text{s}^{-1}$ )	0.98 (0.95 to 0.99)	0.5	0.99 (0.99 to 0.99)	0.4
Sprint Mechanical Properties	$F_0$ (N)	0.87 (0.65 to 0.96)	2.2	0.96 (0.87 to 0.99)	1.9
	$P_{max}$ (W)	0.93 (0.80 to 0.98)	1.9	0.99 (0.96 to 0.99)	1.7
	$v_0$ ( $\text{m}\cdot\text{s}^{-1}$ )	0.98 (0.95 to 0.99)	0.5	0.99 (0.99 to 0.99)	0.4
Hop	CT (s)	0.96 (0.87 to 0.99)	2.4	0.95 (0.85 to 0.98)	2.4
	JH (m)	0.96 (0.87 to 0.99)	2.1	0.94 (0.82 to 0.98)	2.3
	RSI ( $\text{m}\cdot\text{s}^{-1}$ )	0.95 (0.84 to 0.98)	4.6	0.95 (0.86 to 0.98)	4.8
Drop Jump	CT (s)	0.94 (0.83 – 0.98)	3.9	0.96 (0.88 – 0.99)	3.4
	JH (m)	0.96 (0.89 – 0.99)	2.8	0.95 (0.85 – 0.98)	4.5
	RSI ( $\text{m}\cdot\text{s}^{-1}$ )	0.98 (0.94 – 0.99)	2.9	0.95 (0.85 – 0.98)	4.9
Isometric Mid- Thigh Pull	PF (N)	0.96 (0.87 – 0.99)	3.7	0.97 (0.90 – 0.99)	3.4
	Rel PF ( $\text{N}\cdot\text{kg}^{-1}$ )	0.95 (0.86 – 0.99)	3.8	0.94 (0.89 – 0.99)	3.4

$F_0$  = Maximal theoretical horizontal force relative to body mass,  $v_0$  = Maximal theoretical horizontal velocity,

CT = Contact time, JH = Jump height, RSI = Reactive strength index,

PF = Peak force, Rel PF = Peak force relative to body mass.

Table 2: Mean  $\pm$  SD, mean difference with 95% CI, Cohen's d effect size and magnitude for sprint, drop jump, hop and isometric mid-thigh pull.

	Men	Women	Mean Difference (95% CI)	<i>p</i> Value	Effect Size (95% CI)	Magnitude
0-10 m (s)	1.90 $\pm$ 0.05	2.11 $\pm$ 0.10	-0.21 (-0.28 to -0.15)	< <b>0.001</b> **	-2.60 (-3.40 to -1.81)	Very large
10-20 m (s)	1.18 $\pm$ 0.04	1.32 $\pm$ 0.06	-0.15 (-0.18 to -0.11)	< <b>0.001</b> **	-3.08 (-3.86 to -2.30)	Very large
20-30 m (s)	1.09 $\pm$ 0.03	1.24 $\pm$ 0.06	-0.15 (-0.19 to -0.11)	< <b>0.001</b> **	-3.01 (-3.80 to -2.21)	Very large
30-40 m (s)	1.06 $\pm$ 0.05	1.23 $\pm$ 0.07	-0.17 (-0.21 to -0.12)	< <b>0.001</b> **	-2.66 (-3.45 to -1.88)	Very large
40 m (s)	5.22 $\pm$ 0.15	5.90 $\pm$ 0.29	-0.68 (-0.86 to -0.50)	< <b>0.001</b> **	-2.97 (-3.76 to -2.17)	Very large
Max Velocity (m.s <sup>-1</sup> )	9.49 $\pm$ 0.40	8.23 $\pm$ 0.46	1.26 (0.92 to 1.59)	< <b>0.001</b> **	-2.93 (-3.70 to -2.15)	Very large
<i>F</i> <sub>0</sub> (N/kg)	9.3 $\pm$ 0.5	8.0 $\pm$ 0.7	1.4 (0.9 to 1.9)	< <b>0.001</b> **	-2.14 (-2.92 to -1.36)	Very large
<i>P</i> <sub>max</sub> (W·kg <sup>-1</sup> )	22.5 $\pm$ 2.6	16.4 $\pm$ 2.3	6.1 (4.2 to 8.0)	< <b>0.001</b> **	-2.50 (-3.28 to -1.72)	Very large
<i>v</i> <sub>0</sub> (m.s <sup>-1</sup> )	9.84 $\pm$ 0.40	8.51 $\pm$ 0.46	1.33 (1.00 to 1.67)	< <b>0.001</b> **	-3.12 (-3.89 to -2.34)	Very large
Hop CT (s)	0.157 $\pm$ 0.019	0.158 $\pm$ 0.015	-0.001 (-0.014 to 0.012)	0.885	-0.06 (-0.73 to 0.84)	Trivial
Hop JH (m)	0.111 $\pm$ 0.015	0.111 $\pm$ 0.010	0.000 (-0.010 to 0.010)	0.954	-0.02 (-0.76 to 0.81)	Trivial
Hop RSI (m.s <sup>-1</sup> )	0.72 $\pm$ 0.16	0.72 $\pm$ 0.13	0.00 (-0.11 to 0.11)	0.969	-0.01 (-0.79 to 0.76)	Trivial
DJ CT (s)	0.170 $\pm$ 0.028	0.183 $\pm$ 0.028	-0.013 (-0.035 to 0.008)	0.220	-0.47 (-1.25 to 0.30)	Small
DJ JH (m)	0.340 $\pm$ 0.049	0.296 $\pm$ 0.057	0.044 (0.003 to 0.086)	<b>0.038</b> *	0.83 (0.05 to 1.60)	Moderate
DJ RSI (m.s <sup>-1</sup> )	2.06 $\pm$ 0.43	1.65 $\pm$ 0.35	0.41 (0.10 to 0.71)	<b>0.011</b> *	1.04 (0.26 to 1.82)	Moderate
IMTP PF (N)	2642 $\pm$ 437	1913 $\pm$ 342	730 (425 to 1034)	< <b>0.001</b> **	1.86 (1.08 to 2.64)	Large
IMTP Relative PF (N·kg <sup>-1</sup> )	36.3 $\pm$ 6.2	29.8 $\pm$ 5.2	6.49 (2.0 to 10.9)	<b>0.006</b> **	1.13 (0.35 to 1.91)	Moderate

*F*<sub>0</sub> = Maximal theoretical horizontal force relative to body mass, *v*<sub>0</sub> = Maximal theoretical horizontal velocity, CT = Contact time, JH = Jump height

RSI = Reactive strength index, DJ = drop jump, IMTP = Isometric mid-thigh pull, PF = Peak force, Relative PF = Peak force relative to body mass.

\* p<0.05, \*\* p <0.01

0 Correlations between sprint performance variables and sprint mechanical properties and Hop  
 1 RSI, DJ RSI, IMTP PF and IMTP relative PF and are shown in Table 3 and Table 4  
 2 respectively. No significant correlations were found between hop RSI, drop jump RSI, IMTP  
 3 PF or relative PF and any of the sprint performance measures. A significant strong positive  
 4 correlation was found between IMTP PF and relative  $P_{\max}$  in men only.

5

6 Table 3: Inter-correlation matrix between drop jump and hop RSI, isometric mid-thigh pull  
 7 PF and relative PF and sprint performance measures in men (top) and women (bottom).  
 8 Results are presented as  $r$  (95% CI) with statistically significant correlations presented in  
 9 bold.

Men						
	0-10 m (s)	10-20 m (s)	20-30 m (s)	30-40 m (s)	40 m (s)	Max Velocity ( $\text{m}\cdot\text{s}^{-1}$ )
Hop RSI ( $\text{m}\cdot\text{s}^{-1}$ )	-0.22 (-0.67 to 0.35)	-0.15 (-0.63 to 0.42)	-0.22 (-0.67 to 0.35)	-0.17 (-0.65 to 0.39)	-0.21 (-0.67 to 0.36)	0.22 (-0.35 to 0.67)
Drop Jump RSI ( $\text{m}\cdot\text{s}^{-1}$ )	-0.03 (-0.55 to 0.51)	0.01 (-0.52 to 0.54)	0.14 (-0.42 to 0.62)	-0.02 (-0.55 to 0.51)	0.02 (-0.52 to 0.54)	0.10 (-0.46 to 0.60)
IMTP PF (N)	-0.31 (-0.72 to 0.26)	-0.40 (-0.77 to 0.16)	-0.47 (-0.80 to 0.08)	-0.35 (-0.74 to 0.22)	-0.42 (-0.78 to 0.14)	0.30 (-0.27 to 0.72)
IMTP Rel PF ( $\text{N}\cdot\text{kg}^{-1}$ )	-0.31 (-0.72 to 0.26)	-0.29 (-0.71 to 0.29)	-0.24 (-0.68 to 0.34)	-0.22 (-0.67 to 0.35)	-0.30 (-0.71 to 0.28)	0.21 (-0.36 to 0.67)
Women						
	0-10 m (s)	10-20 m (s)	20-30 m (s)	30-40 m (s)	40 m (s)	Max Velocity ( $\text{m}\cdot\text{s}^{-1}$ )
Hop RSI ( $\text{m}\cdot\text{s}^{-1}$ )	-0.34 (-0.74 to 0.23)	-0.16 (-0.64 to 0.40)	-0.31 (-0.72 to 0.27)	-0.22 (-0.67 to 0.35)	-0.28 (-0.71 to 0.29)	0.27 (-0.30 to 0.70)
Drop Jump RSI ( $\text{m}\cdot\text{s}^{-1}$ )	-0.04 (-0.56 to 0.50)	0.21 (-0.36 to 0.67)	0.02 (-0.51 to 0.55)	0.04 (-0.50 to 0.56)	0.04 (-0.50 to 0.56)	-0.03 (-0.55 to 0.51)
IMTP PF (N)	0.30 (-0.27 to 0.72)	0.13 (-0.43 to 0.62)	0.29 (-0.29 to 0.71)	0.36 (-0.21 to 0.75)	0.29 (-0.28 to 0.71)	-0.36 (-0.75 to 0.21)
IMTP Rel PF ( $\text{N}\cdot\text{kg}^{-1}$ )	0.09 (-0.45 to 0.59)	0.01 (-0.52 to 0.54)	0.11 (-0.45 to 0.61)	0.28 (-0.30 to 0.71)	0.13 (-0.43 to 0.62)	-0.24 (-0.68 to 0.34)

RSI = Reactive strength index, IMTP = Isometric mid-thigh pull,

PF = Peak force, Rel PF = Peak force relative to body mass.

10

11

12 Table 4: Inter-correlation matrix between drop jump and hop RSI, isometric mid-thigh pull  
 13 PF and relative PF and sprint mechanical properties in men (top) and women (bottom).

14 Results are presented as r (95% CI) with statistically significant correlations presented in  
 15 bold.

Men			
	$F_0$ (N·kg <sup>-1</sup> )	$P_{max}$ (W·kg <sup>-1</sup> )	$v_0$ (m·s <sup>-1</sup> )
Hop RSI (m·s <sup>-1</sup> )	0.07 (-0.48 to 0.58)	0.15 (-0.42 to 0.63)	0.24 (-0.34 to 0.68)
DJ RSI (m·s <sup>-1</sup> )	-0.11 (-0.60 to 0.45)	-0.23 (-0.68 to 0.34)	0.03 (-0.51 to 0.55)
IMTP PF (N)	0.23 (-0.34 to 0.68)	<b>0.61</b> <b>(0.12 to 0.86)</b>	0.39 (-0.18 to 0.76)
IMTP Rel PF (N·kg <sup>-1</sup> )	0.24 (-0.33 to 0.69)	0.37 (-0.20 to 0.75)	0.24 (-0.33 to 0.68)
Women			
	$F_0$ (N·kg <sup>-1</sup> )	$P_{max}$ (W·kg <sup>-1</sup> )	$v_0$ (m·s <sup>-1</sup> )
Hop RSI (m·s <sup>-1</sup> )	0.34 (-0.24 to 0.73)	0.32 (-0.25 to 0.73)	0.24 (-0.33 to 0.68)
DJ RSI (m·s <sup>-1</sup> )	0.03 (-0.51 to 0.55)	0.00 (-0.53 to 0.53)	0.07 (-0.48 to 0.58)
IMTP PF (N)	-0.13 (-0.62 to 0.43)	-0.27 (-0.70 to 0.31)	-0.33 (-0.73 to 0.24)
IMTP Rel PF (N·kg <sup>-1</sup> )	0.05 (-0.50 to 0.56)	-0.04 (-0.56 to 0.50)	-0.22 (-0.67 to 0.35)

RSI = Reactive strength index, IMTP = Isometric mid-thigh pull, PF = Peak force

Rel PF = Peak force relative to body mass,  $F_0$  = Maximal theoretical horizontal force relative to body mass

$v_0$  = Maximal theoretical horizontal velocity

16

17 The relationships between hop, DJ and IMTP measures for both men and women are shown  
 18 in Table 5. DJ CT had a very large significant correlation with Hop CT, Hop JH and Hop RSI  
 19 in men only. DJ RSI had a significant correlation with Hop CT (men: large negative, women:  
 20 very large negative), Hop JH (men: large positive, women: very large positive) and Hop RSI  
 21 (men and women: large positive). IMTP relative PF had a significant correlation with Hop  
 22 CT (men: large negative), Hop JH (men: large positive) and Hop RSI (men: very large  
 23 positive) and IMTP PF (men and women: very large positive).

24

25

26

27

28 Table 5: Inter-correlation matrix between hop, drop jump and IMTP measures in men (top)  
 29 and women (bottom). Results are presented as r (95% CI) with statistically significant  
 30 correlations presented in bold.

Men					
	DJ CT	DJ JH	DJ RSI	IMTP PF	IMTP Rel PF
	(s)	(m)	(m·s <sup>-1</sup> )	(N)	(N·kg <sup>-1</sup> )
Hop CT (s)	<b>0.84</b> ( <b>0.55 to 0.95</b> )	-0.19 (-0.65 to 0.38)	<b>-0.63</b> ( <b>-0.87 to -0.14</b> )	-0.39 (-0.76 to 0.18)	<b>-0.65</b> ( <b>-0.88 to -0.18</b> )
Hop JH (m)	<b>-0.77</b> ( <b>-0.92 to -0.39</b> )	0.24 (-0.33 to 0.68)	<b>0.63</b> ( <b>0.15 to 0.87</b> )	0.47 (-0.08 to 0.80)	<b>0.68</b> ( <b>0.23 to 0.89</b> )
Hop RSI (m·s <sup>-1</sup> )	<b>-0.77</b> ( <b>-0.92 to -0.41</b> )	0.19 (-0.38 to 0.66)	<b>0.62</b> ( <b>0.14 to 0.87</b> )	0.46 (-0.09 to 0.80)	<b>0.74</b> ( <b>0.34 to 0.91</b> )
IMTP PF (N)	0.01 (-0.52 to 0.54)	0.00 (-0.53 to 0.53)	-0.02 (-0.54 to 0.52)	1	<b>0.86</b> ( <b>0.60 to 0.95</b> )
IMTP Rel PF (N·kg <sup>-1</sup> )	-0.31 (-0.72 to 0.26)	0.19 (-0.38 to 0.66)	0.34 (-0.23 to 0.74)	<b>0.86</b> ( <b>0.60 to 0.95</b> )	1
Women					
	DJ CT	DJ JH	DJ RSI	IMTP PF	IMTP Rel PF
	(s)	(m)	(m·s <sup>-1</sup> )	(N)	(N·kg <sup>-1</sup> )
Hop CT (s)	0.50 (-0.05 to 0.81)	-0.46 (-0.79 to 0.1)	<b>-0.71</b> ( <b>-0.90 to -0.28</b> )	-0.30 (-0.71 to 0.28)	-0.53 (-0.83 to 0.00)
Hop JH (m)	-0.50 (-0.81 to 0.05)	0.47 (-0.08 to 0.80)	<b>0.72</b> ( <b>0.31 to 0.90</b> )	0.28 (-0.30 to 0.70)	0.45 (-0.11 to 0.79)
Hop RSI (m·s <sup>-1</sup> )	-0.42 (-0.78 to 0.14)	0.46 (-0.09 to 0.80)	<b>0.66</b> ( <b>0.20 to 0.88</b> )	0.33 (-0.25 to 0.73)	0.53 (0.00 to 0.83)
IMTP PF (N)	0.13 (-0.43 to 0.61)	0.28 (-0.30 to 0.70)	0.12 (-0.44 to 0.61)	1	<b>0.92</b> ( <b>0.77 to 0.98</b> )
IMTP Rel PF (N·kg <sup>-1</sup> )	-0.01 (-0.54 to 0.52)	0.40 (-0.16 to 0.77)	0.31 (-0.26 to 0.72)	<b>0.92</b> ( <b>0.77 to 0.98</b> )	1

CT = Contact time, JH = Jump Height, RSI = Reactive strength index, DJ = Drop jump

IMTP = Isometric mid-thigh pull, PF = Peak force, Rel PF = Peak force relative to body mass.

31

## 32 DISCUSSION

33 The present study found no significant relationships between drop jump RSI and sprint  
34 performance or sprint mechanical properties in both men and women. In contrast, research in  
35 male sprinters by Smirniotou et al. (37) and female sprinters by Hennessy and Kilty (15)  
36 found significant correlations with sprint acceleration performance over 10, 30 and 60 m.  
37 Young et al. (46) found no relationship with drop jump RSI and sprint performance over 2.5  
38 m and 50 m. The authors, Young et al. (46), suggested that the sprint athletes studied may not  
39 have been able to tolerate the stretch loads imposed on them during the drop jump test. This  
40 may have been the case in the current study as evidenced by the large range of drop jump  
41 CTs (men: 0.137 - 0.249 s, women: 0.144 - 0.227 s) suggesting a wide range of stiffness  
42 capabilities (1). It is likely that drop jump RSI may therefore be a poor indicator of fast SSC

43 performance in groups with wide ranging physical capacities i.e. leg spring stiffness.  
44 Additionally, the ground contact times of the drop jumps in the study were much larger than  
45 those observed during the acceleration (~0.130 s) and transition phase (0.110 – 0.119 s) in  
46 male and female sprint athletes of a similar level (8).

47

48 Similar to drop jumps, no significant relationship was found between hop RSI and any of the  
49 sprint performance or sprint mechanical variables. By contrast, Nagahara et al. (26), found a  
50 relationship between hop RSI and 60 m sprint time, but did not impose a set hopping  
51 frequency on the athletes. Previously, Chelly and Dennis, (6) used a set hopping frequency  
52 (2.0 Hz) and found a large positive correlation ( $r = 0.68$ ) between stiffness and maximal  
53 sprinting velocity. Stiffness measures are considered indicative of an athlete's ability to  
54 tolerate stretch loads and thus achieve shorter CTs (1). The 2.2 Hz frequency used in the  
55 present study resulted in the hopping test becoming a sub-maximal reactive strength test as  
56 athletes limited their jump height in order to maintain the required hopping rhythm. For this  
57 reason, RSI measured in sub-maximal hopping would not reflect an athlete's true ability to  
58 generate an impulse and therefore constrained hopping is not recommended.

59

60 Neither of the IMTP measures was significantly related to any of the sprint performance  
61 measures. This is in contrast to Thomas et al. (39) and West et al. (42) who focused on short  
62 acceleration (20 m) but is in agreement with Wang et al. (41) who assessed longer sprints (40  
63 m). Several key differences exist between those studies and the current study due to the  
64 different populations (sprinters versus team sport players) and different starting procedures  
65 used (block starts versus standing starts). A block start requires substantially greater technical  
66 ability in addition to the need to apply optimal levels of vertical and horizontal force (30). For  
67 the sprint mechanical properties, PF had a significant and large positive correlation with  $P_{max}$   
68 in men with no other significant relationships found. While this may suggest that higher  
69 levels of absolute maximum strength may afford higher levels of horizontal power in  
70 sprinting, this is not supported by the results of the female group and therefore further  
71 research is required before a fully informed conclusion can be made.

72

73 It is important to note that all the strength tests used in this investigation were performed  
74 vertically with no horizontal component and this may partially explain the lack of significant  
75 findings in the current sprinter sample. Weyand et al. (44) found that faster maximum  
76 velocities were achieved predominantly through the application of greater vertical forces



77 (relative to mass) on the ground at very short CTs (~0.100 s). Subsequent research by  
78 Weyand et al. (43) found that the stance phase limit to achieving higher maximum velocities  
79 is imposed by the minimum time required to apply great mass-specific forces and not the  
80 maximum force the limb can apply to the ground. Consequently, the duration of contact  
81 phases during sprinting are not long enough for maximal force production by the lower limb  
82 extensor muscles. The durations of force production in drop jumps, hopping and especially in  
83 the IMTP were considerably longer than those observed at high velocity sprinting.

84

85 The ability to effectively direct the horizontal component of GRF has been shown to be a key  
86 factor in sprint performance. Morin et al. (23) found that the magnitude of the resultant force  
87 was not related to 100 m performance but the ability to direct the action force backwards  
88 against the ground i.e. horizontal force application, was important. In accordance with this,  
89 Rabita et al. (28) found that neither the resultant GRF nor the vertical component were  
90 significantly correlated to sprint performance over 40 m. The authors suggested that the  
91 ability to generate high net horizontal force at high velocity was more important for sprint  
92 acceleration than simply increasing the magnitude of the resultant GRF. The maximal  
93 strength and reactive strength tests in the current study did not examine the athletes' technical  
94 abilities to apply force and therefore the impact of technique on force management could not  
95 be evaluated.

96

97 Differences in sprint performance and mechanical properties between sexes have been well  
98 established in the literature and are consistent with the results of this study. Men generally  
99 achieve faster sprint times due to greater levels of maximal velocity, greater levels of  
100 horizontal force and power, longer acceleration distances, longer step lengths and shorter CTs  
101 (8, 35). Higher  $P_{max}$  and  $F_0$  are likely due to higher muscle mass and larger muscle fiber  
102 cross-sectional areas enabling a greater ability to produce force rapidly, Cheuvront et al. (7).  
103 Furthermore, these differences likely explain the significantly higher IMTP PF and relative  
104 PF observed in men in the current study. The significant differences in drop jump RSI can be  
105 largely attributed to the men attaining moderately higher JHs as differences in CT were  
106 considered small and non-significant.

107

108 No significant sex differences were found in any of the hop variables with CT, JH and RSI  
109 being near identical in men and women. This can be explained by the imposition of a set  
110 hopping frequency inducing an unintended limit on possible RSI scores. A frequency of 2.2

111 Hz constrains total hop time (contact and flight time) to a sum of 0.455 s, therefore the flight  
112 time, which is used to calculate JH, is limited based on the duration of the preceding CT. For  
113 example, a hop with a CT of 0.140 would only permit a flight time of 0.315 s, yielding a JH  
114 limitation to 0.122 m. Shorter CTs are possible in hopping compared to drop jumps since the  
115 imposed stretch loads, which are determined by the athlete's mass and the preceding hop  
116 height, are substantially lower. Consequently, the men and women were equally capable of  
117 tolerating the stretch loads and thus were equally limited in how high they could jump.

118

119 The results of this study indicated that hop CT, JH and RSI had large to very large  
120 correlations with drop jump RSI in both men and women and with IMTP relative PF in men.  
121 All three hop measures had a near perfect relationships with one another (absolute value of r:  
122 0.91 – 0.99) and therefore any variable related to one hop variable would also be related to  
123 the remaining two. This suggests that higher drop jump RSI scores and higher relative PF  
124 values were associated with lower CTs in hopping and subsequently higher JHs and RSI  
125 scores. This highlights the potential role of the drop jump RSI and relative PF as indicators of  
126 an athlete's ability to tolerate relatively low stretch loads in submaximal exercises.

127

128 No relationship was found in the current study between IMTP PF, relative PF and drop jump  
129 RSI in men or women. Barr and Nolte (3) found a significant, moderate positive correlation  
130 between drop jump RSI (from 0.36 m) and 1RM front squat relative to body mass in female  
131 rugby players ( $r = 0.44$ ). Additionally, Beattie et al. (4) found a significant moderate positive  
132 correlation between drop jump RSI (from 0.30 m) and PF measured during an IMTP ( $r =$   
133  $0.30$ ) but no significant correlation between relative PF and RSI, however, the  
134 aforementioned studies did not assess sprint athletes. Both the male and female athletes in the  
135 current study had higher RSI values than the participants in Beattie et al. (4) (Men:  $2.06 \pm$   
136  $0.43$ , Women:  $1.65 \pm 0.35$  versus:  $1.37 \pm 0.31$ ) but considerably lower maximum strength  
137 scores (Men:  $2642 \pm 437$  N, Women:  $1913 \pm 342$  N versus  $3578 \pm 884$  N). This highlights  
138 that high levels of maximum strength are not required to achieve high RSI scores. The higher  
139 RSI scores found in the present sprint athletes were most likely achieved as a result of several  
140 years of sprint and plyometric training.

141

## 142 **PRACTICAL APPLICATIONS**

143 For practitioners who wish to assess reactive strength in hopping, it is recommended that the  
144 test activity should not be constrained by the imposition of a set hopping frequency.

145 Practitioners and researchers are advised to use split times in addition to outcome measures  
146 for studies when investigating correlations because sprint performance is a multidimensional  
147 skill which requires a wide range of physical and technical demands. Furthermore, several  
148 methods of assessing reactive strength are needed that can better represent the demands  
149 present in the distinct phases of sprinting e.g. acceleration, maximum velocity and  
150 deceleration. Finally, it is concluded that greater levels of RSI, as assessed during a 0.3 m  
151 drop jump, do not necessarily require high levels of maximum strength. Training modalities  
152 that utilize movements with CTs below 0.250 s such as sprinting or plyometrics are advised  
153 to enhance fast SSC performance.

154

## 155 **ACKNOWLEDGEMENTS**

156 The authors have no conflict of interest to disclose and would like to thank Rosemary Daniel  
157 for her cooperation with testing and the Irish Research Council for financially supporting this  
158 research.

159

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